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CFD CODE SURVEY FOR THRUST CHAMBER APPLICATION

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ABSTRACT

In the quest to find analytical reference codes, responses from a questionnaire are presented which portray the current CFD program status and capability at various organizations, characterizing liquid rocket thrust chamber flow fields. Sample cases are identified to examine the ability, operational condition, and accuracy of the codes. To select the best suited programs for accelerated further improvements, evaluation criteria are being proposed.

INTRODUCTION

Numerous CFD programs have been developed which characterize liquid rocket thrust chamber flow fields and predict the associated performance. In the past a similar situation existed, leading to a competitive selection process, from which the well known two-dimensional kinetics (TDK) program and several boundary layer codes resulted. These programs were identified as reference programs and still serve in this capacity today. The CFD calculation procedures have not only matched this capability but already provide limited flow process characterizations which exceed the existing recommended methods. A selection of one or several of the best suited programs is of advantage to accelerate the simulation of specific physical mechanisms, where little or no capability exists. Limited funding resources can then be concentrated on these few chosen program candidates.

As indicated at the JANNAF Combustion Meeting at the Marshall Space Flight Center (MSFC) in 1988, a questionnaire was prepared and distributed to the propulsion community with a subsequent good response. A listing of the responding organizations is included in the appendix.

The furnished material has been used to construct a matrix which provides an overview of the operational CFD programs, their physical simulation capabilities, numerical solution techniques, and documentation, to name only a few categories.

In addition to the collected program information, some sample cases are identified which shall be executed by the codes to demonstrate the algorithm maturity and accuracy, and its application to combustion chamber and nozzle flows.

Of consequence are the presented criteria below, which may be used in the selection process for the most qualified CFD codes. This is projected to occur during the 1992/93 time frame. The parties planning to participate in the development of a reference program are requested to review the proposed selection approach and provide their comments, critique, or consent.

OBJECTIVE

The presented material should inform the propulsion community of the various existing CFD computer program capabilities and their operational status. This is the first step in a process leading eventually to the selection of the most advanced code(s) for the prediction of thrust chamber flow fields and the associated performance. Exposure of the programs to particular sample cases and a final test, with unknown results to the program operators, will be further milestones during this process. The identified sample cases and the proposed program evaluation criteria should be reviewed by the parties involved.

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QUESTIONNAIRE RESULTS

The overall response to a questionnaire, which I prepared and distributed in the beginning of 1989, was very satisfactory, but extended over a long time period. Therefore, an update of the original information was initiated in September 1990 to include the most recent advances of the programs in question. The important information has been organized down to a very detailed level, and the results are presented in Table 1. It shall be noted that only problems related to the operation of liquid rocket thrust chambers, composed of the combustion chamber and the nozzle, are of concern here.

The key topics in Table 1 address the foundation of the code, followed by the physical process simulation capability, and the numerical solution methods used. The categories thereafter reflect primarily the validation status of the code, experience and success with specific problems, ease of preparing a case, and supporting elements to evaluate and display the results. Finally, information with regard to the program documentation, code availability, and computer oriented questions is displayed. The abbreviations shown in the columns represent abridged forms of the actual terminology which can be interpreted without difficulty by the readers who are somewhat familiar with the subject. Assistance in this matter can be found in Table 2.

From the survey it is evident that the CFD codes have achieved already a high level of physical process simulation; however, the advanced models are scattered in the matrix of Table 1. Examples of such advanced techniques refer to turbulence modeling via large eddies, spectral method discretization, jet breakup calculation, and droplet interaction in the spray regime. It is anticipated that the presented information will motivate the program developers to equip their codes with the latest methods.

BENCHMARK TESTING

It is the responsibility of every CFD code developer to expose his program to the most commonly known simple benchmark tests and prove that the program works for the basic flow simulation and the physical model features. Under basic features the treatment of incompressible, compressible, inviscid, laminar, low to high Mach number, shock capturing, two-dimensional, three-dimensional, steady state, time dependent, and geometry or grid dependent flows is normally recognized, while the simulation of turbulence, atomization, two-phase spray, vaporization, multi-species with chemical reactions, and heat transfer refers to the physical modeling.

SAMPLE CASES

To examine the program capability, maturity, and accuracy with respect to a thrust chamber flow simulation, the execution of sample cases shown in Table 3 is recommended. These sample cases are related to the basic flow conditions in a combustion chamber and nozzle, but also reflect situations which have been experienced in the past and which are of utmost importance. Attention is focused on the injector region, where flows from different injection elements produce a spray, sometimes with intentional stream striation arrangements for performance optimization and hardware protection. The flow pattern adjacent to the wall contour is another important domain in which turbulence dominates the viscous behavior and the heat transfer process. Based on the engine operation cycle, such as a regeneratively cooled concept or an expander cycle approach, the wall design and the near wall flow conditions serve different functions and are very different indeed. Thrust chamber flow start and shut-down, which are feed system driven, as well as the nozzle exhaust flow, interacting with the ambient air, are highly important conditions which need to be firmly comprehended.

To start this project, it is planned to form a group of experts from the government and industry shortly, which will provide explicit details for the uniform treatment of recommended sample cases. Initial and boundary conditions, basic and physical flow features, and recommended grids to run these cases will be specified. The format of the results for individual parameter, tabular, and graphic presentation will be identified also. Program solutions will be collected and compared with available measurements or other recognized data. The organizations which continue to advance their CFD programs are encouraged to participate in this activity.

CFD CAPABILITY GOAL

Ultimately, the requirements for a comprehensive CFD program, simulating the flow motion in a thrust chamber, must include the characterization of bi-propellants and two-phase flow undergoing liquid jet atomization, vaporization, propellant mixing, chemical reaction, flow expansion from low to high Mach numbers, viscous effects, and heat transfer processes. Steady-state and transient flow modeling for three-dimensional flows are mandatory. In the fluid spray regime the interaction between neighboring droplets must be simulated, especially for conditions below and above the critical point. Nozzle flow interaction with the ambient air during captive testing and during flight from the launch site to vacuum conditions in orbit is also imperative.

At this time, the developed computer programs use specific assumptions to overcome the deficiencies in the previously quoted areas of physical process descriptions more or less successfully. Experimental research programs and associated modeling activities are constantly underway to eliminate these shortcomings gradually. However, the new formulations are frequently 'hardwired' into the codes, and a transfer to other programs for technology sharing is rather difficult. To exchange advanced techniques quickly and efficiently, the new routines should be structured in modules with clearly identified interface parameters. Such an approach offers a special advantage when specific techniques, numerical or physical, need to be examined for their efficiency and accuracy. Using standard parameter nomenclature will definitely be effective.

Since some domains in a thrust chamber flow field require simulation with extensive details of the physical processes, while other areas are much simpler in character and can be described with less effort, a decoupling of the entire flow field at beneficial interfaces may offer an advantage and should be explored. One such interface could be at a place in the combustion chamber where the spray flow terminates and the expansion process starts. Here, the particular information of the entire injection process, which has been obtained from a detailed CFD solution, may be transferred to a subsequent quick and efficient CFD analysis. Certainly, a fully coupled solution is the goal; however, the provision of an interface, from a position of problem complexity and current computer limitations in core and execution time, should not be disregarded.

SELECTION CRITERIA

The selection of one or several CFD programs to serve as reference codes is of paramount importance and must be conducted fairly. Subsequently, rules and guidelines are presented for review by the propulsion community. Additional topics with weighing factors, ranging from 1 to 10 (highest), are welcome. A panel of government experts only, acceptable to the propulsion community, will collect all verbal and written comments and formulate the decisive selection criteria. The final ranking procedure of the topics will not be disclosed. Every organization can participate in this competition and will be subject to the following recommended criteria:

- A government person with a competing CFD program cannot serve on this panel.
- The selected codes and documentation must be available unconditionally.
- The candidate program must execute specific test cases which will be announced by the panel in the future.
- Program application strength to thrust chamber flows will be evaluated.
- Solution accuracy will be assessed.
- Specific simulation features will be appraised.
- User friendliness will be studied.
- Validation status will be reviewed, based on benchmark and sample cases.
- Code competence will be assessed with respect to documented problem results.
- Quality of the program documentation will be surveyed.
- Interaction with other supporting programs, such as preprocessor, grid generator, and postprocessor, including graphics display will be checked.
- Computer oriented topics will be rated (program size, vectorized, etc.)
- Background, experience, and skill of the program developer(s) will be reviewed.
- After selection, new developed routines must be announced and distributed on request.
- The selected codes will serve as reference programs. In this capacity the data can be used for comparison with other code results for validation.

SUMMARY

Information, related to the current CFD program capabilities and provided by various organizations, has been compiled and presented. Specific sample cases for thrust chamber flow demonstration capability are recommended to promote code advancements and validation. The analytical potential of a future comprehensive code has been stated, and the anticipated steps leading to the selection of the best interim candidates have been introduced. The communication between a panel of CFD oriented experts and the propulsion community will review the recommended selection criteria and formulate a final set with associated weighing of the topics. The selection process is projected to occur in the 1992/93 time period.

ACKNOWLEDGEMENT

I wish to acknowledge the support and assistance of Dr. Sura Kim from SVERDRUP, Inc. (Support Contractor to MSFC) during the many discussions leading to the evaluation matrix format, the evaluation of the submitted material, and the typing of the entire table. My thanks also go to Dr. Don Bai and Mr. Huu Trinh, both from MSFC, for their enduring and spirited contribution in this matter.

APPENDIX

ACUREX	Acurex Corporation
AEROJET	Aerojet TechSystems Company
ARGONNE	Argonne National Laboratory
CHAM	CHAM of North America, Inc.
CFDRC	CFD Research Corporation
CREAREX	Creare.X
HSC	Huntsville Sciences Corporation
NASA/ARC	NASA, Ames Research Center
PRI	Physical Research, Inc.
P&W	Pratt & Whitney
REMTECH	Remtech, Inc.
ROCKETDYNE	Rocketdyne
SEA	Software and Engineering Associates
SECA	Software Engineers, Consultants, Analysts
SRA	Scientific Research Associates, Inc.
UAH	University of Alabama, Huntsville
UCI	University of California, Irvine
UIC	University of Illinois, Chicago
UTSI	University of Tennessee, Space Institute

TABLE 3. SAMPLE CASES

- Thrust chamber using O_2/H_2 , O_2/C_2H_4 propellants
- Combustion chamber equipped with a turbulence ring
- Thrust chamber with tangential flow injection in axial direction
- Combustion chamber with flow injection in circumferential direction
- Thrust chamber with a striated mixture ratio profile
- Thrust chamber with separated nozzle flow
- Thrust chamber with sharp throat radii of curvature
- Combustion chamber with unconventional geometry (inclined injector face, tapered walls, small contraction ratio)
- Combustion chamber with various types of injection patterns
- Thrust chamber with heat transfer to the wall for a given temperature profile
- Thrust chamber with regenerative coolant flow
- Thrust chamber with transpiration cooling
- Time dependent thrust chamber start and shut-down operation

TABLE 1. QUESTIONNAIRE RESULTS

Table 1 (1a)		ACUREX	AEROJET	ARGONNE**	CFDRC	CHAM
ORGANIZATION		A. Murray	T. Nguyen	G. Berry	S.Habchi/A.Przekwas	Mahaffey/Vlachos
RESPONS. PERSON		KIVA-G	BICOMB	GEMCHIP	REFLEQS	PHOENICS
CODE NAME		3D	2D,Axisymmetric	2D	2D,3D	1D,2D,3D
DIMENSIONS		Cart,BdyFit	BdyFit		BdyFit(all)	Cart,Cyl,BdyFit
COORDINATES	CART/CYL/SPH/BODY FIT	Unsteady	Stdy	Unsteady	Stdy,Unsteady	Stdy,Unsteady
TIME PROBLEM	STEADY/UNSTEADY	Vis(L/T)	Vis(-/T)	Vis(-/T)	Invis,Vis(-/T)	Invis,Vis(L/T)
TYPE OF FLOW	INVISCID/VISCID	Incomp,Cmp(all)	Cmp(slb/Tr)	Incomp,Cmp(Sb)	Incomp,Cmp(Sb/Tr/Sp)	Incomp,Cmp(Sb/Tr/S)
EQUATIONS	INCOMP/COMPRESSIBLE	Consrv			Consrv	Consrv
	CONSERV/NONCONSERV	N-S(Incomp/Cmp)	N-S(Cmp)		N-S	N-S
	MOMENTUM	Yes	Yes	Yes	Yes	Yes
	ENERGY	Yes(7)	Yes(3 max)	Yes(7)	Yes(4 step reaction)	Yes(35+)
PHYSICAL PROCESS	SPECIES	E-L	E-E	E-E	E-L	E-E,E-L(opt)
	MULTI PHASES TRACKING	R.G.(Eqn)	I.G.	I.G.,R.G.(Eqn)	R.G.(7)	I.G.,R.G.(7)
	EQUATION OF STATE	Eqn	Eqn	Eqn	Tabl,Eqn	Tabl,Eqn
	TRANSPORT PROPERTIES	K			B-L(TBD)	MixL
	TURBULENCE MODELING		KeH	KeH	KeH,KeL	KeH
	ATOMIZATION MODEL	Calcu	Asmnd(Imput)	Asmnd	Asmnd,Calcu	
	VAPORIZATION MODEL	Drplet(M)	Yes(7)	Yes(7)	Drplet(S/M)	Crit(Sup)
	CHEMISTRY MODEL	FR	FR	FR	EQ,FR	EQ,FR
	RADIATION MODEL				Yes(6 flux eqn)	6 Flux Model
ROCKET PROPELLANT	TYPE	General(7)	all		HC/Air,Hypersonic	HC/Air,O2
DISCRETIZATION	PHASES(FUEL/OX)	Multi(G/L)	Two(G/G,G/L)	Two(L/G,L/L)	Sgl,T(G/G,G/L,L/L)	Two(7)
	FDM/FVM/FEM/SPECTRAL/ETC.	FVM	FVM	FVM	FVM	FVM
NUMERICAL SCHEME	VARIABLES BASED	P-V		P-V	P-V	P-V
	DIFF. ACCURACY:TIME/SPATIAL	T(1st)/S(1st,2nd)	T(7)/S(2nd)		T(1st)/S(1st,2nd)	T(7)/S(1st,2nd)
MATRIX SOLVER	MULTI STEP/FACTORIZATION					MS(No)/FACT(Yes)
	EXPLICIT	Explicit(Temporal)				No
	IMPLICIT	Implicit(Spatial)		Fully Implicit	Fully Implicit	Implicit
	OTHERS: SPECIFY	ALE			TVD	
			SIMPLER	SIMPLER	SIMPLEC	SIMPLEST,IPSA
	MULTIGRID CAPABILITY	No			No	No
	DIRECT METHOD	Not Req'd	TDMA	TDMA	Mod. Stone's solver	Stone's solvr
	ITERATIVE METHOD		Line Iter	Line Iter		

Survey Date : October, 1990 (Except **)

TABLE 1. QUESTIONNAIRE RESULTS

Table 1 (1b)

ORGANIZATION		ACUREX	AEROJET	ARGONNE**	CFDRC	CHAM
RESPONS. PERSON		A. Murray	T. Nguyen	G. Berry	S.Habchi/A.Przekwas	Mahaffey/Vlachos
CODE NAME		KIVA-G	BICOMB	GEMCHIP	REFLEQS	PHOENICS
GRID	SEPARATE (NAME)	GGP			EAGLE,GGP(opt)	GGP,Others
	INTERNAL	Northo	Sigg,Northo	Ortho	Ortho/Northo	Sigg,Ortho/Northo
			Struct	Adapt	Struct	Struct
INLET/WALL BOUNDARY COND.	TECHNIC USED	N/A	Algr		Algr	Algr,Diff
	INLET CONDITIONS	Const	Const		Const,TimeVar	Const,TimeVar
	WALL BOUNDARY	Usr specify	Nalp	Nalp	Usr Select.	Slp/Nalp,MV/Fix
PROGRAM CAPABILITY (Experienced)		Adiab,Isoth	Adiab	Adiab		Adiab,Isoth,Flux
		Surf(S)	Surf(S)	Handl Interior B.C.	Handl Interior B.C.	Handl Interior B.C.
		Adh			Adh,Bounce	
CODE VALIDATION	INCOMPRESSIBLE FLOWS				Swirl, Rotation flow	All
	COMPRESSIBLE FLOWS	0.1 - 24	0.1 - 20		0 - 65	All
	INTERNAL FLOW	Recirc,Cavity	Separ,Recirc		Separ,Recirc,Cavity	All
PRE/POST PROCESSOR		Combustor,Nozz	Combustor,Nozz	Spray combustion	Combustor,Nozz	Combustor,Nozz
	INJECTION	Coaxial			Yes(?)	
		Atom,Vapor	Mix,Vapor		Atomiz,Vapor,Mix	
PROGRAM	PERFORMANCE PREDICTION	Therm,Dyn Prop	All	Therm,Dyn prop	Thrust,Lsp,Dyn prop	All
	MISC.	Plume,Shock tube			Duct	Duct
	UNIQUE CASES	13			40	~ 200
COMPUTER SYSTEM	CASES PUBLISHED	7			30	~ 25
	THRUST CHMBR RELATED	5			4	~ 5
	DEVELOPED	Inhouse	Inhouse	N/A	Inhouse	Inhouse,Others
MISCELLANEOUS	OPERATION	Batch	Batch,Interact		Batch,Interact	Interact
	GRAPHICS	DI300,DISSPLA	DI3000,Plot3D	N/A	Plot3D,XYPLOT	Self,PATRAN,Spns
	DOCUMENTATION	Eng,User	N/A(TBD)	TBD	Eng,Prog,User	Eng,Prog,User
COMPUTER SYSTEM	AVAILABILITY	Prop	Prop	Pub(Argonne)	Prox	Sale
	MAIN FRAME	Cray	Cray	Cray,IBM	Cray,IBM	Cray,IBM,Cyb
	MINI COMPUTER	Vax	Vax	Vax	Alliant,Ardent,Vax	Convex,Alliant,Vax
MISCELLANEOUS	WORKSTATION		SG		Sun	Sun,Apollo,Tek
	CODE EXPERIENCE	2 Yrs	1 Yrs	4 Yrs	4 Yrs	9 Yrs
	CODE ORIGIN	Acq(KIVA)	Acq(GEMCHIP)	Inhouse	Inhouse	Inhouse
MISCELLANEOUS	VECTORIZATION	Yes	No		Yes	Yes

Survey Date : October, 1990 (Except **)

TABLE 1. QUESTIONNAIRE RESULTS

Table 1 (2a)

ORGANIZATION		CREARE.X	CREARE.X	CREARE.X	HSC	NASA,ARC
RESPONS. PERSON		Z. Sheikh	S. Subbiah	S. Subbiah	L. Spradley	S. Yoon/D. Kwak
CODE NAME		FLUENT	RAMPANT	NEKTON	PACES	CENS3D
DIMENSIONS		2D,3D	2D,3D	2D,3D	2D,3D	2D,3D
COORDINATES	CART/CYL/SPH/BODY FIT	Cart,Cyl,BdyFit	BdyFit	BdyFit	BdyFit	BdyFit
TIME PROBLEM	STEADY/UNSTEADY	Stdy,Unstdy	Stdy,Unstdy	Unstdy	Unstdy	Stdy,Unstdy
TYPE OF FLOW	INVISCID/VISCID	Invis,Via(L/T)	Invis,Via(L/T)	Invis,Via(L)	Invis,Via(L/T)	Invis,Via(L/T)
	INCOMP/COMPRESSIBLE	Incomp,Cmp(Sb/Tr/Sp)	Cmp(Sb/Tr/Sp)	Incomp	Cmp(?)	Cmp(all)
EQUATIONS	CONSERV/NONCONSERV	Consrv	Consrv	NonConsrv	Consrv	Consrv
	MOMENTUM	N-S	N-S_Eul	N-S	N-S(Cmp)	N-S(-/Cmp)
	ENERGY	Yes	Yes	Yes	Yes	
	SPECIES	Yes(unlimit)		No	Yes(30)	Yes(11)
	MULTI PHASES TRACKING	E-L				
	EQUATION OF STATE	I.G.	I.G.		I.G.,R.G.(Tabl)	R.G.(Eqn)
	TRANSPORT PROPERTIES	Tabl,Eqn		Eqn	Eqn	Eqn
PHYSICAL PROCESS	TURBULENCE MODELING					B-L
		KeH	KeH		KeH/KeL	
		AST,RSM				
	ATOMIZATION MODEL	Asmnd				
	VAPORIZATION MODEL	Drplet(S/M)				
	CHEMISTRY MODEL	EQ,FR			FR	FR
	RADIATION MODEL	Discrete Trans				
ROCKET PROPELLANT	TYPE				H2/O2,HC/Air	Air/H2
	PHASES(FUEL/OX)	Sngl(S/G)			Sngl	
DISCRETIZATION	FDM/FVM/FEM/SPECTRAL/ETC.	FVM	FVM	Spectral	FEM	FVM
NUMERICAL SCHEME	VARIABLES BASED	P-V	D-V	P-V	D-V	D-V
	DIFF. ACCURACY:TIME/SPATIAL	T(1st)/S(1st)	T(1st)/S(2nd)	T(3rd)/S(15th)	T(2nd)/S(2nd)	T(1st)/S(2nd)
	MULTI STEP/FACTORIZATION	MS(No)/FACT(No)			MS(Yes)/FACT(No)	MS(No)/FACT(Yes)
	EXPLICIT			Adam-Baschworth	FEM-FCT	
	IMPLICIT					Yoon-Jameson
	OTHERS: SPECIFY				ALE,Tay-Gal,FCT	TVD
		SIMPLE				
	MULTIGRID CAPABILITY	No		Yes	No	Yes
MATRIX SOLVER	DIRECT METHOD	TDMA		Tensor Product		
	ITERATIVE METHOD	Iter		CGM	Iter	G-S(LU-SGS)

Survey Date : October, 1990 (Except **)

TABLE 1. QUESTIONNAIRE RESULTS

Table 1 (2b)

ORGANIZATION		CREARE.X	CREARE.X	CREARE.X	HSC	NASA,ARC
RESPONS. PERSON		Z. Sheikh	S. Subbiah	S. Subbiah	L. Spradley	S. Yoon/D. Kwak
CODE NAME		FLUENT	RAMPANT	NEKTON	FACES	CENS3D
GRID	SEPARATE (NAME)	PREFL	PREFL	PRENEK		GGP
	INTERNAL	Sigs,Northo	Nsgg,Northo	Nsgg,Northo		Ortho/Northo
		Strct	Unstrct,Adapt	Unstrct	Unstrct,Adapt	Adapt,MultZon
INLET/WALL BOUNDARY COND.	TECHNIC USED	Algr,Diff	Algr	FEM	FEM	Algr,Diff
	INLET CONDITIONS	Const,TimeVar	Const	Const,TimeVar	Const,TimVar,Char	Const,TimeVar
	WALL BOUNDARY	Slp/Nslp,MV/Fix	Slp/Nslp,MV/Fix	Slp/Nslp,MV/Fix	Nslp,Mv	Nslp
PROGRAM CAPABILITY (Experienced)		Adiab,Isoth,Flux	Adiab,Isoth,Flux	Adiab,Isoth,Flux	Isoth	Nonreflecting cond
		Surf(S/R)	Surf(S)	Surf(S)	Surf(S)	
		Adh,Bounce,Salts(7)				
CODE VALIDATION	INCOMPRESSIBLE FLOWS	0.1 - 1.0E12		Laminar-Trans	1.0E2 - 1.0E8	
	COMPRESSIBLE FLOWS	0.1 - 5.0	0.3 - 5.0	< 0.3		0.1-30
	INTERNAL FLOW	Recirc,Separ	Separ,Recirc	Separ,Recirc	Separ,Recirc	Separ
PRE/POST PROCESSOR		Combustor,Nozz			Combustor,Nozz	Inlet/Combustor
	INJECTION	Coax,Impinge				
		Vapor,Mix				
PROGRAM	PERFORMANCE PREDICTION				Therm,DynProp,Isr	Therm,Dyn Prop
	MISC.				WaveImpinge,Aero	Hypersonic Vehicle
	UNIQUE CASES	250			10	
COMPUTER SYSTEM	CASES PUBLISHED	30			25	
	THRUST CHMBR RELATED				2	
	DEVELOPED	Inhouse	Inhouse	Nektonics	Inhouse,Others	Inhouse
MISCELLANEOUS	OPERATION	Batch,Interact	Batch,Interact	Batch,Interact	Batch,Interact	Interact
	GRAPHICS	Self	Self	Self	Self,SG-IRIS	GAS,SURF,Plot3D
	DOCUMENTATION	Eng,Prog,User	Eng,Prog,User	Eng,Prog,User	N/A	
COMPUTER SYSTEM	AVAILABILITY	Salc	Salc,Prop	Salc	SBIR	Pub
	MAIN FRAME	Cray,IBM	Cray,IBM	Cray,IBM	Cray,Cyb	Cray
	MINI COMPUTER	Convex,Alliant,Vax	Convex,Alliant,Vax	Convex,Alliant	Vax,Convex	Vax
MISCELLANEOUS	WORKSTATION	Sun,Apollo,Tek	Sun,Tek	Sun,Apollo,Tek	SG,UNIX	SG
	CODE EXPERIENCE	8 Yrs	1 Yrs	4 Yrs	3 Yrs	2 Yrs
	CODE ORIGIN	Inhouse	Inhouse	Acq(MIT)	Acq(PEFLO)	Inhouse
MISCELLANEOUS	VECTORIZATION	No	No	Yes	Yes	Yes

Survey Date : October, 1990 (Except **)

TABLE 1. QUESTIONNAIRE RESULTS

Table 1 (3a)

ORGANIZATION		P & W	P & W	PRI	PRI	REMTECH
RESPONS. PERSON		D. Hill	C. Rhie	Dang/Kehamavaz	Dang/Kehamavaz	S.Praharaj/P. Liver
CODE NAME		ARICC	NASTAR	NSI	UPNS	PARCREM
DIMENSIONS		2D,Axiymmetric	2D,3D	2D	2D	2D,3D
COORDINATES	CART/CYL/SPH/BODY FIT		BdyFit	BdyFit	BdyFit	BdyFit
TIME PROBLEM	STEADY/UNSTEADY	Unstdy	Stdy	Unstdy	Stdy	Stdy,Unstdy
TYPE OF FLOW	INVISCID/VISCID	Invis,Vis(L/T)	Invis,Vis(L/T)	Vis(-/T)	Vis(-/T)	Invis,Vis(L/T)
	INCOMP/COMPRESSIBLE	Cmp(Sb)	Incomp,Cmp(all)	Cmp(7)	Cmp(7)	Cmp(all)
EQUATIONS	CONSERV/NONCONSERV	Consrv	Consrv			Consrv
	MOMENTUM	N-S	N-S,PNS,Eul	N-S(Cmp)	PNS	NS(Cmp),TLNS,Eul
	ENERGY	Yes	Yes	Yes	Yes	Yes
	SPECIES	Yes(11 max)	Yes(4,5,7)		Yes(40)	Yes(9)
	MULTI PHASES TRACKING	E-L				
	EQUATION OF STATE	I.G.	I.G.,R.G.(Tabl)	I.G.	I.G.,R.G.(Cp=C)	I.G.,R.G.(Eqn)
	TRANSPORT PROPERTIES	Eqn	Tabl,Eqn		Tabl	Eqn
PHYSICAL PROCESS	TURBULENCE MODELING	MixL(SGS)	B-L	Cebeci-Smith	Cebeci-Smith	B-L
		KeH	KeH,KeL		KeH	KeL
	ATOMIZATION MODEL	Asmtd				
	VAPORIZATION MODEL	Drplet(S/M)				
	CHEMISTRY MODEL	EQ,FR	FR		FR	EQ
	RADIATION MODEL			No		
ROCKET PROPELLANT	TYPE	H2/O2	H2/O2,HC			H2/O2
	PHASES(FUEL/OX)	Two(G/L)			Sngl	Sngl(gas)
DISCRETIZATION	FDM/FVM/FEM/SPECTRAL/ETC.	FVM	FVM	FDM	FDM	FDM
NUMERICAL SCHEME	VARIABLES BASED	P-V	P-V	D-V	D-V	D-V
	DIFF. ACCURACY:TIME/SPATIAL	T(1st)/S(1st)	T(7)/S(2nd)	T(7)/S(2nd)	T(7)/S(2nd)	T(2nd)/S(2nd)
	MULTI STEP/FACTORIZATION		MS(Yes)/FACT(No)			MS(Yes)/FACT(Yes)
	EXPLICIT					
	IMPLICIT	Implicit	Implicit			B-W
	OTHERS: SPECIFY	ALE		TVD	TVD	ADI
			PISO			
	MULTIGRID CAPABILITY	No	Yes			No
MATRIX SOLVER	DIRECT METHOD		SLOR TDMA	BTDMA	BTDMA	Pentadiagonal Slvr
	ITERATIVE METHOD	Point solver-?	Iter			

Survey Date : October, 1990 (Except **)

TABLE 1. QUESTIONNAIRE RESULTS

Table 1 (3b)

ORGANIZATION		P & W	P & W	PRI	PRI	REMTECH
RESPONS. PERSON		D. Hill	C. Rhie	Dang/Kehrmavaz	Dang/Kehrmavaz	S.Praharaj/P. Liver
CODE NAME		ARICC	NASTAR	NSI	UPNS	PARCREM
GRID	SEPARATE (NAME)		OGP			INGRID
	INTERNAL	Stgg,Northo	Nstgg,Northo			
			Strct,MultZone			Strct,Adp,MultZon
INLET/WALL BOUNDARY COND.	TECHNIC USED	Algbr	FEM,Algbr,Diff	Algbr	Algbr	Algbr
	INLET CONDITIONS	Const	Const			Const,TimeVar
	WALL BOUNDARY	Nslp	All		Nslp	Nslp,MV
		Iscth	All			Adiab,Iscth
		Surf(S)	Surf(S)			Surf(S)
		Bounce				
	PROGRAM CAPABILITY (Experienced)		1.0E0 - 1.0E8			1.0E2 - 1.0E8
	COMPRESSIBLE FLOWS		0.0 - 30			0.4 - 33
CODE VALIDATION	INTERNAL FLOW		All			Separ,Recirc,Cavity
			Combustor,Nozz	Nozz	Combustor,Nozz	Nozz
	INJECTION	Coax	All			
		Atomiz,Vapor,Mix				
	PERFORMANCE PREDICTION	Dyn Prop		All	All	Therm,Dyn prop
	MISC.					Ext flow,Plume
	UNIQUE CASES	8	300			> 20
	CASES PUBLISHED	4	30			> 10
	THRUST CHMBR RELATED	-	100			5
	PRE/POST PROCESSOR	Inhouse(Post)	Inhouse,Others	N/A	N/A	Inhouse
PROGRAM	OPERATION	Batch	Batch			Batch,Interact
	GRAPHICS	Plot3D,Self	Plot3D,Self	Calcomp	Calcomp	Plot3D,DISSPLA
	DOCUMENTATION	User	User	N/A	Eng,User	Eng,User
	AVAILABILITY	Pub-MSFC	Prop	Pub	Pub(TBD)	Pub,Prop(some)
COMPUTER SYSTEM	MAIN FRAME	Cray	Cray			Cray
	MINI COMPUTER			Vax	Vax	Convz,Multiflow
	WORKSTATION			Sun	Sun	Sun
MISCELLANEOUS	CODE EXPERIENCE	2 Yrs	6 Yrs	1 Yrs	1.5Yrs	4 Yrs
	CODE ORIGIN	Acq(ARICC)	Inhouse	Inhouse	Inhouse	Acq(PARC)
	VECTORIZATION	Yes(Parts)	Yes			Partially

Survey Date : October, 1990 (Except **)

TABLE 1. QUESTIONNAIRE RESULTS

Table 1 (4a)

ORGANIZATION		ROCKETDYNE	SEA	SECA	SRA	UAH
RESPONS. PERSON		P.Y. Liang	D. Costa	Y. Chen	J. Sabnis	C.P. Chen
CODE NAME		ARIC3D	VIPER	FDNS	CELMINT	MAST
DIMENSIONS		2D,3D	2D	2D,3D	2D,3D	
COORDINATES	CART/CYL/SPH/BODY FIT	BdyFit	BdyFit	BdyFit	BdyFit	BdyFit
TIME PROBLEM	STEADY/UNSTEADY	Unsteady	Stdy	Stdy,Unsteady	Stdy(opt),Unsteady	Unsteady
TYPE OF FLOW	INVISCID/VISCID	Vis(-/T)	Invis,Vis(L/T)	Invis,Vis(L/T)	Vis(-/T)	Invis,Vis(-/T)
	INCOMP/COMPRESSIBLE	Cmp(?)	Cmp(?)	Incmp,Cmp(Sb/Ts/Sp)	Incmp(opt),Cmp(?)	Incmp,Cmp(?)
EQUATIONS	CONSERV/NONCONSERV		Consrv	Consrv	Consrv	Consrv
	MOMENTUM	N-S(-/Cmp)	PNS	N-S(Incmp/Cmp)	N-S(-/Cmp)	NS(Incmp/Cmp),Eul
	ENERGY	Yes	Yes	Yes	Yes	Yes
	SPECIES	Yes(?)	Yes(40)	Yes(compl. memory)	Yes(?)	Yes(?)
	MULTI PHASES TRACKING	E-L	-	E-E,E-L	E-E,E-L	E-L,Stat
	EQUATION OF STATE	I.G.,R.G.(Cp=C)	R.G.(?)	R.G.(Eqn)	I.G.,R.G.(Tabl)	I.G.,R.G.(Eqn)
	TRANSPORT PROPERTIES	Eqn	Eqn	Tabl,Eqn	Eqn	Eqn
PHYSICAL PROCESS	TURBULENCE MODELING	SGS	Cebeci-Smith		MixL	
		KeH2-Scale	KeH	KeH,KeL	KeL	KeH,KeL
				ASM		Multi-Scale Model
	ATOMIZATION MODEL	Yes		Asamd		Asamd
	VAPORIZATION MODEL	Yes		Drplet(S/M)	Drplet(S)	Drplet(S/M),Crit(Sb)
	CHEMISTRY MODEL	EQ,FR	EQ,FR	EQ,FR	FR,Statistic. Model	EQ
	RADIATION MODEL			Yes(?)		-
ROCKET PROPELLANT	TYPE	H2/O2,HC/O2	All	H2/O2,HC/O2,Other		H2/O2
	PHASES(FUEL/OX)	Two(G/L)	(1) Sngl,Two	Two(G/G,G/L,G/S)	Sngl,Two(G/L,G/S)	Two(G/S,G/L)
DISCRETIZATION	FDM/FVM/FEM/SPECTRAL/ETC.	FVM	FDM	FDM	FDM,FVM	FVM
NUMERICAL SCHEME	VARIABLES BASED			P-V	D-V	P-V
	DIFF. ACCURACY:TIME/SPATIAL	T(1st)/S(1st,2nd)	S(2nd)	T(2nd)/S(4th)/w/ Diss	T(1st,2nd)/S(2nd)	T(2nd)/S(2nd)
	MULTI STEP/FACTORIZATION	MS(Yes)/FACT(No)		MS(Yes)/FACT(No)	MS(No)/FACT(Yes)	MS(Yes)/FACT(No)
	EXPLICIT					
	IMPLICIT	Implicit	B-W	Time-Centered	B-McD	
	OTHERS: SPECIFY	ALE		C-N,TVD	Block ADI	
		SOLA-VOF		Multi-Correctors		PISOC
	MULTIGRID CAPABILITY	No	No	Yes	No	Yes
MATRIX SOLVER	DIRECT METHOD		TDMA	Stone's solvr	BTDMA	
	ITERATIVE METHOD	CRM		or Line Iter.		CGM(CGS)

Survey Date : October, 1990 (Except **)

(1) Equil. gas particle mixture

TABLE 1. QUESTIONNAIRE RESULTS

Table 1 (4b)

ORGANIZATION		ROCKETDYNE	SEA	SECA	SRA	UAH
RESPONS. PERSON		P.Y. Liang	D. Coats	Y. Chen	J. Sabnis	C.P. Chen
CODE NAME		ARIC3D	VIPER	FDNS	CELMINT	MAST
GRID	SEPARATE (NAME)	GGP		EAGLE,GENIE,GR	EAGLE,GGP	
	INTERNAL	Stgg,Northo		Nstgg,Northo	Northo,Moving	Northo
		Stret,Adp	Stret	Unstret,MultZone	Adapt,MultZon	
	TECHNIC USED	Algr	Algr	Algr,Diff		Diff
INLET/WALL	INLET CONDITIONS	User Specify	Const	Const,TimeVar	Const,TimeVar	Const,TimeVar
	BOUNDARY COND.	User Specify	Nslp	Slp/Nslp	User specify	Nslp,MV
			Adiab,Flux	Adiab,Isent,Flux		Const,TimeVar
			Surf(S)	Surf(S)	Handl Interior B.C.	Surf(S)
PROGRAM CAPABILITY (Experienced)				Adh,Bounce	Adh,Bounce	Adh,Bounce
	INCOMPRESSIBLE FLOWS		1.0E3 - 1.0E7	0.1 - ∞	1.0-1.0E7	1.0E1 - 1.0E6
	COMPRESSIBLE FLOWS	0 - 6	1.0 - 10	0.0 - 20	1.0E-4 - 20	0.1 - 8
	INTERNAL FLOW	Separ,Recirc,Cavity		Recirc,Cavity,Separ	Ballistic,Cavity	Separ,Recirc,Cavity
CODE VALIDATION	INJECTION	Combustor,Nozz	Nozz	Combustor,Nozz	RocketMotor,Nozz	
		Coax,Transverse		Coax		Coax
		Atomiz,Vapor,Mix			Vapor,Mix	Vap,Mix
	PERFORMANCE PREDICTION	Therm Prop	All	All	Therm,Dyn Prop	
	MISC.	Pipe flow,BwdStep		Duct,Turbblad,Plum	Ext flow(tz/Hyper)	
	UNIQUE CASES		8	46	40	15
	CASES PUBLISHED		8	29	25	10
	THRUST CHMBR RELATED		8	7		0
PRE/POST PROCESSOR	DEVELOPED	Inhouse/Others	Inhouse,Post	Inhouse	Others	Inhouse
	OPERATION	Batch(?)	Batch	Batch	Batch,Interact	Batch
	GRAPHICS	DISPLA,Self	Self	Self,Plot3D	Plot3D	Display
	DOCUMENTATION	User(2D only)	Eng,User	User	Eng,Prog,User	Eng,Prog
COMPUTER SYSTEM	AVAILABILITY	Prot	Pub	Pub	Prop,Sale,Prot,Pub	Pub
	MAIN FRAME	Cray		Cray,IBM	Cray,Cyb	Cray
	MINI COMPUTER	FPS	Vax	Avion	Vax	
	WORKSTATION	Sun	Sun		Sun,SG	Sun
MISCELLANEOUS	CODE EXPERIENCE	1 Yrs	Developing	4 Yrs	14 Yrs	Developing
	CODE ORIGIN	Acq(KIVAILARICC)	Inhouse	Inhouse	Inhouse	Inhouse
	VECTORIZATION	Yes	No	Partially	Yes	No

Survey Date : October, 1990 (Except **)

TABLE 1. QUESTIONNAIRE RESULTS

Table 1 (5a)

ORGANIZATION		UCI	UIC**	UTSI	UTSI**	RCKTDYNE
RESPONS. PERSON		R. Rangel	P. Chiu	S. Jeng	F. Collins	M. Sindir
CODE NAME		SHEET2	GEMCHIP LILII	ABC(KIVA-II)	CASP(PARC)	USA
DIMENSIONS		2D	3D	3D	2D,Axisymmetric	
COORDINATES	CART/CYL/SPH/BODY FIT	Cart		BdyFit	BdyFit	
TIME PROBLEM	STEADY/UNSTEADY	Unstdy	Stdy,Unstdy	Unstdy	Stdy	Unstdy
TYPE OF FLOW	INVISCID/VISCID	Invis	Vis(-/T)	Vis(L/T)		Invis,Vis(-/T)
	INCOMP/COMPRESSIBLE	Incomp	Cmp(7)	Cmp(Sb)		Incomp,Cmp(all)
EQUATIONS	CONSERV/NONCONSERV			Consrv	Consrv	
	MOMENTUM	N-S(Incomp)-Vort	N-S(Cmp)	N-S(Cmp)	N-S(Cmp),Eul	N-S(Incomp/Cmp)
	ENERGY	(1).		Yes		
	SPECIES	Yes(4)	Yes(7)	Yes(30)		
	MULTI PHASES TRACKING	E-L	E-E	E-L		
	EQUATION OF STATE	I.G.	I.G.,R.G.(7)	R.G.(Eqn)	I.G.	R.G.(Eqn)
	TRANSPORT PROPERTIES	Eqn		Eqn	Eqn	Eqn
PHYSICAL PROCESS	TURBULENCE MODELING				B-L	B-L,K
		LES	Modified KeH	KeH		KeH
	ATOMIZATION MODEL	Asamd	Asamd	Asamd		
	VAPORIZATION MODEL	Drplet(S/M)	(1),(2) Drplet(7)	Crit(Sub/Sup)		
	CHEMISTRY MODEL	TBD	FR	EQ,FR	EQ	FR
	RADIATION MODEL	TBD	TBD			
ROCKET PROPELLANT	TYPE	HC		MMH/N2O2	H2/O2	
	PHASES(FUEL/OX)	Two(7)	Multi(G/G,L/G,L-L/G)	Two(L/L)	Sngl	
DISCRETIZATION	FDM/FVM/FEM/SPECTRAL/ETC.	FDM-Scalar	FVM	FVM	FVM	FVM
NUMERICAL SCHEME	VARIABLES BASED	Lagrangian manner		P-V		
	DIFF. ACCURACY:TIME/SPATIAL	2nd Runge-Kutta	T(-)/S(1st)	T(1st)/S(2nd)	T(-)/S(2nd)	
	MULTI STEP/FACTORIZATION				MS(No)/FACT(Yes)	MS(Yes)/FACT(Yes)
	EXPLICIT	Explicit				Explicit(R-K)
	IMPLICIT		Fully implicit		B-W	Implicit
	OTHERS: SPECIFY			ALE		TVD/Riemann
			SIMPLER			
	MULTIGRID CAPABILITY	No		No		
MATRIX SOLVER	DIRECT METHOD	TDMA	TDMA		Pentadiagonal solvr	TDMA,BTDMA
	ITERATIVE METHOD		Line Iter	CGM		

Survey Date : October, 1990 (Except **)

(1) Vorticity field eq' (1) Droplet dispersion model

(2) Group/Conjugate effects included

TABLE 1. QUESTIONNAIRE RESULTS

Table 1 (5b)

ORGANIZATION		UCI	UIC**	UTSI	UTSI**	RCKTDYNE
RESPONS. PERSON		R. Rangel	P. Chin	S. Jeng	F. Collins	M. Sindir
CODE NAME		SHEET2	GEMCHIP I,II,II	ABC(KIVA-II)	CASP(PARC)	USA
GRID	SEPARATE (NAME)	Cartesian(?)	Preselected grid		INGRID	Norho
	INTERNAL		Ortho	Ortho/Norho		Src,Multizone
				Adapt(TBD)		
	TECHNIC USED			Diff		
	INLET/WALL	Must be assumed		Const	Usr specify	Usr Specify
	BOUNDARY COND.		Fix	Slp/Nalp	Need stat file	
		No Walls	Adiab,Flux	Adiab,IsotH,Flux		
		Handl Periodic B.C.		Surf(S/R)		
				Adh,Bounce		
PROGRAM CAPABILITY (Experienced)	INCOMPRESSIBLE FLOWS	1.0E1 - 1.0E2				
	COMPRESSIBLE FLOWS			0.1-1.2	-33	
	INTERNAL FLOW					Cavity
			Combustor	Rocket		Combustor,Nozz
	INJECTION				Nozz	
		Vapor,Mix				
	PERFORMANCE PREDICTION	Vorticity,Velocity	Therm,Dyn Prop	Therm		Therm,Dyn Prop
	MISC.				Ext.flow,Duct,etc	Ext.flow(Sup,Hyp)
	UNIQUE CASES	5		5		
	CASES PUBLISHED	5		2		
CODE VALIDATION	THRUST CHMBR RELATED			2		
	DEVELOPED	Inhouse	Others	N/A	Others	Inhouse
	OPERATION		Batch	Batch		Interact
PROGRAM	GRAPHICS	GPR,Self		Plot3D	Plot3D	Self
	DOCUMENTATION	N/A	TBD	N/A		Usr
	AVAILABILITY		Prop, Pub	Prop		Prop
COMPUTER SYSTEM	MAIN FRAME		Cray		Cray	Cray,Cyb
	MINI COMPUTER			Alliant	Multiflow	Convex
	WORKSTATION	Apollo	Sun		Sun	Sun
MISCELLANEOUS	CODE EXPERIENCE	2 Yrs	6/4/2 Yrs	1 Yrs	3 Yrs	4 Yrs
	CODE ORIGIN	Inhouse	Inhouse	Acq(KIVA II)	Acq(PARC)	Inhouse
	VECTORIZATION	No		Yes		

Survey Date : October, 1990 (Except **)

TABLE 2. ABBREVIATIONS

COORDINATES	CART,CYLIN,SPHER,BODY FIT	Cart,Cyl,Sph,BdyFit
TIME PROBLEM	STEADY/UNSTEADY	Stdy,Unstdy
TYPE OF FLOW	INVISCID/VISCID	Invis,Vis(L/T)
	INCOMPRESSIBLE/COMPRESSIBLE	Incomp,Comp(Subsonic/Transonic/Supersonic/Hypersonic)
EQUATIONS	CONSERV/NONCONSERV FORM	Consrv,Nconsv
	MOMENTUM/ENERGY/SPECIES	N-S(Incomp/Comp),PNS,Euler// Energy(Max. Number of species)
	MULTI PHASES TRACKING	E-E-L-Stat
	EQUATION OF STATE	I.G.,R.G.(Tabl/Eqn)
	TRANSPORT PROPERTIES	Tabl,Eqn
PHYSICAL PROCESS	TURBULENCE MODELING	MixL,B-L,K,K-1,KEH,
	ATOMIZATION MODEL	KeL,LES,PDF,ASM,RSM
	VAPORIZATION MODEL	Assmd,Calcu,Vorti
	CHEMISTRY MODEL	Drplet(S/M),Crit(Sub/Sup)
	RADIATION MODEL	No,EQ,FR
ROCKET PROPELLANT	TYPE	Flame,Wall
	PHASES(FUEL/OX)	H2/O2,HC/O2
DISCRETIZATION	FDM/FVM/FEM/SPECTRAL/ETC	Sngl,Two(G/G,G/L,S/G)
NUMERICAL SCHEME	DIFF. ACCURACY:TIME/SPATIAL	FDM,FVM,FEM,SP
	MULTI STEP/FACTORIZATION	T(1st)/S(2nd)
	EXPLICIT	MS(Yes,No)/FACT(Yes,No)
	IMPLICIT	L/D-F,L-W,MacC,Hop,etc.
	OTHERS	MacC,B-W,B-McD
	VARIABLES BASED	Crank-Nicolson,ADI,TVD,ALE/ICE-ALE,Flux Correct Transport,Taylor-Galerkin
	MULTIGRID CAPABILITY	SIMP,PISO,SOLA
MATRIX SOLVER	DIRECT METHOD	P-V,D-V,Others
	ITERATIVE METHOD	Yes/No
GRID	SEPARATE (NAME)	TDMA,Block TDMA,Error Vector Prop.,etc.
	INTERNAL	Line Iter.,Gauss-Seidel,SOR,Conjugate Gradient/Residue Method,etc.
	TECHNIC USED	EAGLE,GRID,Grid Generation Package,etc.
BOUNDARY CONDITION	INLET/WALL BOUNDARY	Stagg/Non-Stagg,Ortho/Non-Ortho,Struct/Ustruct,Adaptive Grids/Multi Zone
		FEM,Algebraic,Differential Eqn
PROGRAM CAPABILITY	INCOMPRESSIBLE FLOWS	Inlet: Constant,Time Varying; Wall: No slip/Slip,Stationary/Moving,
(Experienced)	COMPRESSIBLE FLOWS	Adiabatic,Isotherm,Const. Flux,Smooth/Rough Surface,etc.
	INTERNAL FLOW	DropIet wall interaction(Adhere/Bounce/Others)
	INJECTION	Specify Reynolds No. Ranges
	PERFORMANCE PREDICTION	Specify Mach No. Ranges
	MISC.	Separating,Recirculating,Cavity Flows,etc.
CODE VALIDATION	UNIQUE/PUBLISHED CASES	Combustion Chamber,Nozzle
	THRUST CHAMBER RELATED	Element-Coaxial/Impingement, Process-Atomization/Mixing/Vaporization
PRE/POST PROCESSORS	DEVELOPED	Thrust Chamber:Thrust,Lap,Thermodynamic Properties,Dynamics Properties
	GRAPHICS	Other than Thrust Chamber
PROGRAM	OPERATION	Number of Unique Cases Solved(Include benchmark cases)/No. of Publications
	DOCUMENTATION	Number of Cases related to Thrust Chamber
COMPUTER SYSTEM	AVAILABILITY	In-house,By Others
	MAIN FRAME	Display,Plot3D,Self,etc.
	MINI COMPUTER	Batch,Interactive
	WORKSTATION	Manual-Engineering,Program,User
MISCELLANEOUS	CODE EXPERIENCE	Proprietary,Sale,Protect(SBIR),Public Domain
	ORIGIN	Cray,IBM,Cyber,etc.
	VECTORIZATION	Convex,Alliant,Vax,etc.
		Sun,Apollo,Tek,SiliconG,etc.
		No. of years Used
		In-house,Acquired(Original Code name)
		Programed for Vectorization(Yes/No)
		Yes/No

PAGE 1